

# Ka-Band Monolithic InGaAs/InP HBT VCO's in CPW Structure

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**Abstract**—Two Ka-Band monolithic voltage controlled oscillators (VCO's) designed in coplanar waveguide (CPW) structure are described in this letter. Each VCO utilizes a InGaAs/InP heterojunction bipolar transistor (HBT) as the active device and a HBT base-collector junction as the tuning varactor. These two VCO's are biased at a very low voltage of  $V_{CE} = 1.5$  V and the emitter current is less than 10 mA. Under this low dc power dissipation, the VCO's with center frequencies of 26.5 and 33.5 GHz show high dc-to-rf conversion efficiencies over 10% and 5% within the frequency tuning ranges of 1.6 and 1.2 GHz, respectively. The measured phase noise at 1 MHz offset frequency is  $-110$  dBc/Hz.

## I. INTRODUCTION

As the wireless communications of voice, video, and data grows, the increasing demand of channels and bandwidths is driving the transceiver systems toward millimeter-wave frequencies. Currently, there are several applications in Ka-band and 60 GHz [1]. Low phase-noise oscillator with high efficiency is a key component in the transceiver front end. III-V HBT's with low  $1/f$  noise and high efficiency are suitable active devices for building oscillators at microwave and millimeter-wave frequencies [2], [3].

Recently, Ka-band MMIC VCO's using GaAs- or InP-based HBT technology were demonstrated [4]–[6]. A GaInP/GaAs HBT VCO at 28 GHz with phase noise of  $-65$  dBc/Hz at 100 kHz off carrier and tuning bandwidth of 5.5 GHz was reported [4]. Using the same material structure, a 35 GHz VCO with phase noise of  $-80$  dBc/Hz at 100 kHz off carrier and tuning bandwidth of 1 GHz was fabricated [5]. In addition to the GaAs-based HBT VCO, an InP-based (InAlAs/InGaAs) HBT VCO at 31 GHz was reported without phase noise characteristics [6].

In this letter, we report on InGaAs/InP HBT VCO's at 26.5 and 33.5 GHz. Phase noise levels at 100 kHz and 1 MHz offset frequencies are  $-80$  dBc/Hz and  $-110$  dBc/Hz, respectively. With a low dc bias voltage of 1.5 V and low current of less than 10 mA, the dc-to-rf conversion efficiencies for the VCO's at 26.5 and 33.5 GHz is higher than 10% and 5%, respectively. The coplanar waveguide (CPW) structure, which eliminates the processing of via holes, is first introduced into the Ka-band MMIC VCO design.

## II. DESIGN

The oscillators were designed in a CPW structure using common base configuration. Two separate VCO's designated

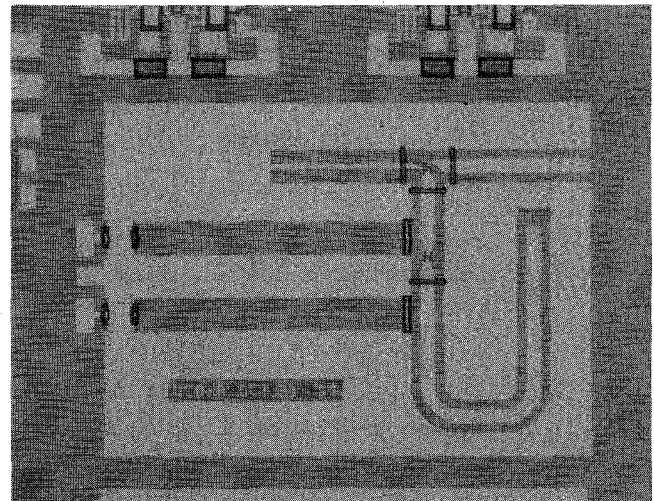


Fig. 1. Photograph of VCO-A (26.5 GHz).

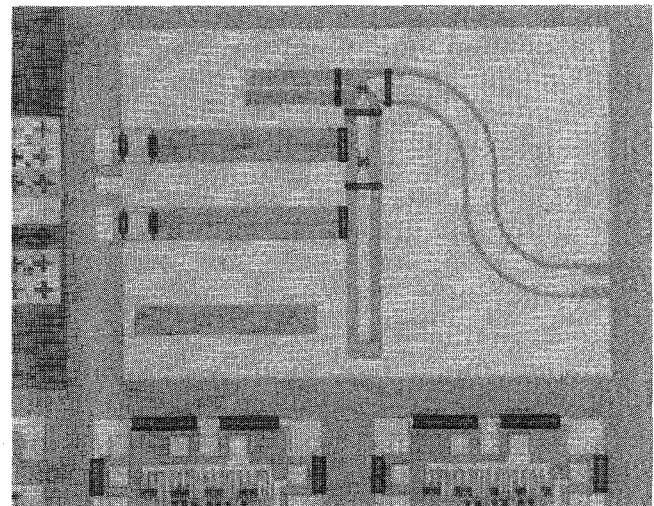


Fig. 2. Photograph of VCO-B (33.5 GHz).

A and B were designed for 26.5 GHz (Fig. 1) and 33.5 GHz (Fig. 2). The base is connected to the ground through a CPW short-circuited stub. A varactor utilizing the base-collector junction of a transistor is inserted in the resonant tank connected to the emitter of the HBT. The collector is connected to the VCO output port via a section of CPW line for impedance matching. Cross-over bridges are placed near junctions of transmission lines to avoid the excitation of even mode (coupled slot mode). High impedance CPW lines and Metal-Insulator-Metal (MIM) capacitors were used as dc bias

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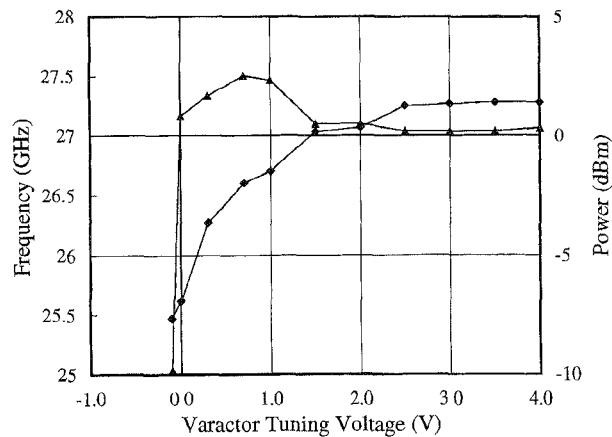


Fig. 3. Frequency tuning and output power of VCO-A.  $\blacklozenge$ —: Frequency;  $\blacktriangle$ —: Power.

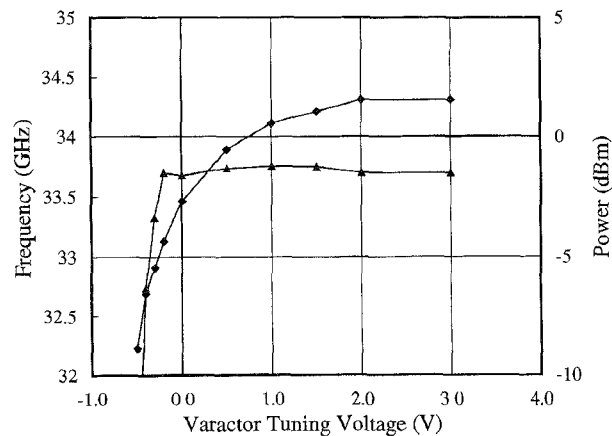


Fig. 4. Frequency tuning and output power of VCO-B.  $\blacklozenge$ —: Frequency;  $\blacktriangle$ —: Power.

lines. The chip size is  $1.75 \text{ mm} \times 1.2 \text{ mm}$  for both VCO-A and VCO-B.

### III. FABRICATION

The InGaAs/InP HBT wafers were grown in the Metal-Organic Molecular Beam Epitaxy (MOMBE) system. The HBT device used in the VCO has an emitter size of  $3 \mu\text{m} \times 10 \mu\text{m}$ . The collector doping and thickness are  $1 \times 10^{16} \text{ cm}^{-3}$  and 500 nm, respectively. The short-circuited current gain cutoff frequency  $f_T$  is 100 GHz and the maximum oscillation frequency  $f_{\text{max}}$  is greater than 60 GHz. The maximum available gain at 30 GHz is 7 dB with a collector current of 15 mA.  $\text{SiO}_2$  is used for passivation as well as the dielectric layer of MIM capacitor. To reduce the parasitic capacitance and support the cross-over bridges, polyimide with thickness of  $1 \mu\text{m}$  is used. Since the ground plane is on the same side of the circuitry, no via hole processing is needed.

### IV. RESULT

Frequency tuning and output power were measured at the bias condition of  $V_{\text{CE}} = 1.5 \text{ V}$  ( $V_{\text{BE}} = 1.0 \text{ V}$  and  $V_{\text{CB}} = 0.5 \text{ V}$ ). The emitter current  $I_E$  was 6.8 mA for VCO-A and 9.5 mA for VCO-B. The result is shown in Figs. 3 and 4. The

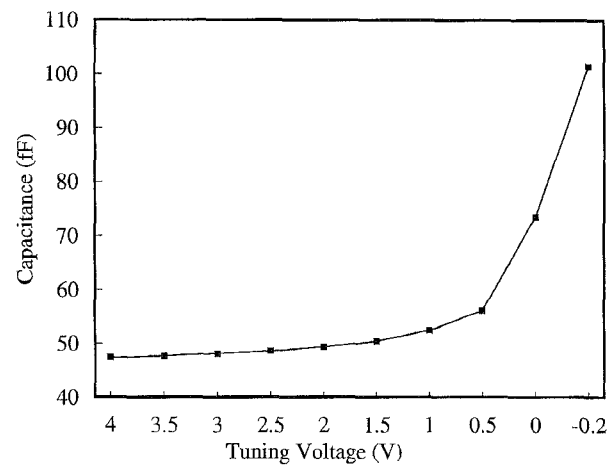


Fig. 5. Capacitance tuning performance of varactor diode.

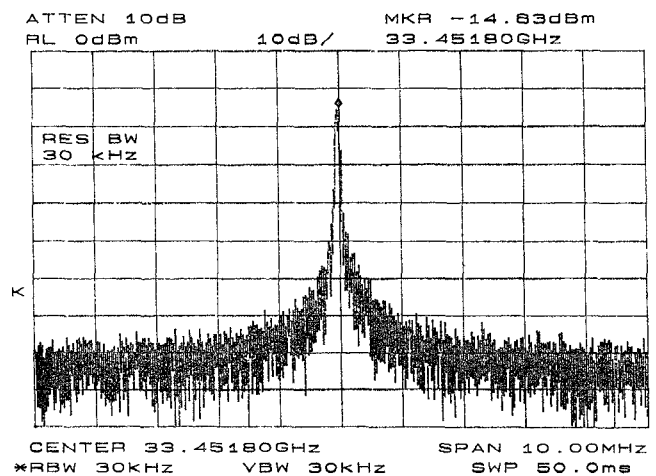


Fig. 6. Output spectrum of VCO-B at 33.45 GHz.

capacitance tuning performance of varactor is shown in Fig. 5. The tuning capacitance ratio is 1.5:1 from 0 to 4 V for VCO-A and 2.1:1 from  $-0.2$  to 3 V for VCO-B. The frequency tuning range of VCO-A is 1.6 GHz and the output power varies from 0.2 to 2.5 dBm. For VCO-B, the frequency tuning range is 1.2 GHz and the output power is within  $-1.43 \pm 0.2 \text{ dBm}$ . The overall dc-to-rf conversion efficiency within the tuning range is 10% for VCO-A and 5% for VCO-B. At tuning voltage of 0.7 V, the conversion efficiency of VCO reaches 17% at 26.6 GHz. An output spectrum of VCO-B is shown in Fig. 6. The measured phase noise levels at 100 kHz and 1 MHz offset frequencies are  $-81$  and  $-112 \text{ dBc/Hz}$  for VCO-A and  $-79$  and  $-107 \text{ dBc/Hz}$  for VCO-B.

The output power of the circuit increases as  $V_{\text{CE}}$  and  $I_C$  increase. With the constrained bias voltage of  $V_{\text{CE}} = 1.5 \text{ V}$ , however, the HBT VCO's designed here are not optimized for output power but for a combination of dc-to-rf conversion efficiency, phase noise, and frequency tuning range.

### V. CONCLUSION

Monolithic Ka-band VCO's were developed using InGaAs/InP HBT and CPW circuit design. Frequency tuning ranges of VCO's with center frequencies at 26.5 and 33.5

GHz are 1.6 and 1.2 GHz, respectively. DC-to-rf conversion efficiencies of 10% and 5% were achieved with a low dc bias voltage  $V_{CE} = 1.5$  V and emitter current less than 10 mA. The features of low dc power dissipation, high efficiency, and low phase noise enable this HBT VCO technology to be applied in low-power wireless communications.

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